

1. Estimate the power transmission capacity of a muff coupling having shaft diameter of 80 mm , muff diameter of 150 mm rotating at 150 rpm . $[\tau]_{\text{shaft}} = 50 \text{ N/mm}^2$. $[\tau]_{\text{muf}} = 10 \text{ N/mm}^2$

SOLUTION:-

- $d = 80 \text{ mm}$
- $D = 150 \text{ mm}$
- $N = 150 \text{ rpm}$
- $[\tau]_{\text{shaft}} = 50 \text{ N/mm}^2$
- $[\tau]_{\text{muf}} = 10 \text{ N/mm}^2$
- $P = \text{????}$

$$M_t = \frac{\pi}{16} d^3 \times [\tau]$$

$$= (\text{pie}/16) * 80^3 * 50$$

$$= 5.02 * 10^6 \text{ N*mm}$$

$$M_t = 5.02 * 10^3 \text{ N*m}$$

POWER P

$$P = \frac{2\pi N M_t}{60 \times 10^3}$$

$$= 2 * \text{PIE} * 5.02 * 10^3 * 150 / 60$$

$$= 78.85 * 10^3 \text{ watt}$$

$$= 78.85 \text{ KW}$$

$$P = \frac{2\pi N M_t}{60 \times 10^3} \quad 5.02 \times 10^6$$

2. A hollow shaft having 230 mm and 310 mm internal and external diameter respectively rotates at 120 rpm and transmits 30hp. Determine the stresses induced in the shaft.

Solution:-

- D = 310 mm
- d = 230 mm
- N = 120 RPM
- P = 30 HP = 30 * 0.746 = 22.38 KW
- $\tau = \text{????}$

1. Torque:-

$$M_t = \frac{\text{KW} \times 10^6 \times 60}{2\pi N} \quad (\text{N.mm})$$

$$= 22.38 * 10^6 * 60 / (2 \pi * 120)$$

$$= 1780943.81 \text{ N}\cdot\text{mm}$$

2. Shear stress:-

$$M_t = \frac{\pi}{16} \left[\frac{D^4 - d^4}{D} \right] \times [\tau]$$

$$\tau = M_t * 16 * D / (\pi * (D^4 - d^4))$$

$$= 1780943.81 * 16 * 310 / (\pi * (310^4 - 230^4))$$

$$= 0.33 \text{ N/mm}^2$$

3. A flange coupling transmit 15 Kw power at 200 rpm. Maximum torque is 25 % higher than full load torque. Determine the diameter of shaft and number of bolts. $[\tau]_{\text{shaft}} = 40 \text{ N/mm}^2$.

Solution:

➤ $P = 15 \text{ KW}$

➤ $N = 200 \text{ RPM}$

➤ $T_{\text{max}} = T + 25\%T = 1.25 * T$

➤ $d, n = \text{????}$

1. Find shaft dia;-

$$M_t = \frac{\text{KW} \times 10^6 \times 60}{2\pi N} \text{ (N}\cdot\text{mm)}$$

$$= 15 * 10^6 * 60 / (2 \pi * 200)$$

$$= 716.19 * 10^3 \text{ N}\cdot\text{mm}$$

$$T_{\max} = 1.25 * T$$

$$= 1.25 * 716.19 * 10^3$$

$$= 895.24 * 10^3 \text{ N} * \text{mm}$$

$$M_t = \frac{\pi}{16} * d^3 * [\tau]_{\text{shaft}}$$

$$d^3 = 16 * T_{\max} / (\pi * \tau_{\text{shaft}})$$

$$= 16 * 895.24 * 10^3 / (40 \pi)$$

$$d^3 = 113.98 * 1000 \text{ mm}$$

$$= 48.46 \text{ mm}$$

$$= 50 \text{ mm}$$

2. No. of bolt

$$n = 0.02d + 3$$

$$= 0.02 * 50 + 3$$

$$n = 4$$

4. Find the diameter for the 4 bolts of a flange coupling to transmit 60kW at 300rpm. The pitch circle diameter of bolt is 300mm. The allowable shear stress

for bolt is 25MPa. Assume maximum torque to be 25% greater than full load torque.

Solution:-

➤ $n = 4$

➤ $P = 60 \text{ KW}$

➤ $N = 300 \text{ RPM}$

➤ $D_p = 300 \text{ mm}$

➤ $[\tau]_{\text{bolt}} = 25 \text{ MPa} = 25 \text{ N/mm}^2$

➤ $T_{\text{max}} = 1.25 * T$

➤ $d_b = \text{????}$

1. Find Torque;-

$$\begin{aligned} M_t &= \frac{\text{KW} \times 10^6 \times 60}{2\pi N} \text{ (N.mm)} \\ &= 60 * 10^6 * 60 / (2 \pi * 300) \\ &= 1.90 * 10^6 \text{ N*mm} \end{aligned}$$

$$\begin{aligned} T_{\text{max}} &= 1.25 * T \\ &= 1.25 * 1.90 * 10^6 \\ &= 2.375 * 10^6 \text{ N*mm} \end{aligned}$$

2. Dia of bolt:-

$$[M_t] = \frac{\pi}{4} \times d_b^2 \times [\tau]_{\text{bolt}} \times n \times \frac{D_P}{2}$$

$$\therefore d_b = \left[\frac{8 \times [M_t]}{\pi \times [\tau]_{\text{bolt}} \times n \times D_P} \right]$$

$$= 8 \times 2.375 \times 10^6 / (\pi \times 25 \times 4 \times 300)$$

$$d_b = 14.19 \text{ mm}$$

$$= 16 \text{ mm}$$

5. A simple flange coupling has to transmit 40 KW at 450 RPM. Assume torque to be 25 % more than the full load. Calculate (a) Shaft diameter (b) Key Dimensions and (c) number & size of Bolts. The stresses are as under, For Shaft & Key $\sigma = 100 \text{ N/mm}^2$, $\tau = 50 \text{ N/mm}^2$ & $\tau_c = 75 \text{ N/mm}^2$ For Bolt $\tau_b = 40 \text{ N/mm}^2$.

SOLUTION:

- $P = 40 \text{ KW}$
- $T_{\text{max}} = 1.25 \times T$
- $N = 450 \text{ RPM}$
- $\sigma = 100 \text{ N/mm}^2$ (shaft & key)
- $\tau = 50 \text{ N/mm}^2$ (shaft & key)
- $\tau_b = 40 \text{ N/mm}^2$

➤ $d, L, W, t, n, d_b = \text{?????}$

1. FIND SHAFT DIAMETER (d):-

$$\begin{aligned}M_t &= \frac{KW \times 10^6 \times 60}{2\pi N} \text{ (N.mm)} \\&= 40 \times 10^6 \times 60 / (2\pi \times 450) \\&= 848.82 \times 10^3 \text{ N*mm}\end{aligned}$$

$$\begin{aligned}T_{\max} &= 1.25 * T \\&= 1.25 * 848.82 * 10^3 \\&= 1.06 * 10^6 \text{ N*mm}\end{aligned}$$

$$\begin{aligned}M_t &= \frac{\pi}{16} \times d^3 \times [\tau] \\d^3 &= 16 * T_{\max} / (3.14 * \tau_{\text{shaft}}) \\&= 16 * 1.06 * 10^6 / (3.14 * 50) \\d &= 47.62 \text{ mm} \\&\mathbf{d = 48 \text{ mm}}\end{aligned}$$

2. KEY DIMENSIONS:-

- $L = 1.57d = 1.57 * 48 = 75.36 \text{ mm} = 76 \text{ mm}$
- $W = d/4 = 48/4 = 12 \text{ mm}$
- $T = d/6 = 48/6 = 8 \text{ mm}$

3. BOLT DIMENSIONS :-

➤ Pitch circle diameter $D_1 = D_p = 3d = 3 * 48 = 144$ mm

➤ **No of bolt $n = 0.02d + 3 = 0.02*48 + 3 = 3.96 = 4$ nos.**

➤ Diameter of bolt d_b :

$$[M_t] = \frac{\pi}{4} \times d_b^2 \times [\tau]_{\text{bolt}} \times n \times \frac{D_p}{2}$$

➤ $\therefore d_b = \left[\frac{8 \times [M_t]}{\pi \times [\tau]_{\text{bolt}} \times n \times D_p} \right]$

$$= 8 * 1.06 * 10^6 / (3.14 * 40 * 4 * 144)$$

$$= 10.82 \text{ mm}$$

$d_b = 12$ mm

6. A C.I. flange coupling is required to transmit 15 kW at 900 R.P.M. Find shaft diameter 'd', hub diameter 'D', no. of bolts 'n' and bolt diameter 'db'. Permissible stresses - shear $[\tau]$ for shaft and bolt material = 40 Mpa and crushing stress for bolt material = 80 Mpa and shear stress for C.I. flange material $[\tau] = 8$ MPa.

1. FIND SHAFT DIAMETER (d):-

$$M_t = \frac{KW \times 10^6 \times 60}{2\pi N} \text{ (N.mm)}$$

$$= 15 * 10^6 * 60 / (2\pi * 900)$$

$$= 159.15 * 10^3 \text{ N*mm}$$

$$M_t = \frac{\pi}{16} \times d^3 \times [\tau]$$

$$d^3 = 16 * T_{\max} / (3.14 * \tau_{\text{shaft}})$$
$$= 16 * 159.15 * 10^3 / (3.14 * 40)$$

$$d = 27.26 \text{ mm}$$

$$\mathbf{d = 28 \text{ mm}}$$

3. FIND HUB DIAMETER (D):-

$$D = 2d = 2 * 28 = 56 \text{ mm}$$

$$M_t = \frac{\pi}{16} \left[\frac{D^4 - d^4}{D} \right] \times [\tau]$$

$$\tau_{\text{hub}} = 16 * M_t * D / (3.14(D^4 - d^4))$$
$$= 16 * 159.15 * 10^3 * 56 / (3.14(56^4 - 28^4))$$
$$= 4.92 \text{ N/mm}^2$$

If, $\tau_{\text{hub}} \leq [\tau_{\text{hub}}]$ then design is safe

4. BOLT DIMENSIONS :-

- Pitch circle diameter $D_1 = D_p = 3d = 3 * 28 = 84 \text{ mm}$
- **No of bolt $n = 0.02d + 3 = 0.02 * 28 + 3 = 3.56 = 4 \text{ nos.}$**
- Diameter of bolt d_b :

$$[M_t] = \frac{\pi}{4} \times d_b^2 \times [\tau]_{\text{bolt}} \times n \times \frac{D_P}{2}$$

$$\Rightarrow \therefore d_b = \left[\frac{8 \times [M_t]}{\pi \times [\tau]_{\text{bolt}} \times n \times D_P} \right]$$

$$= 8 \times 159.15 \times 10^3 / (3.14 \times 40 \times 4 \times 84)$$

$$= 5.49 \text{ mm}$$

$$\mathbf{d_b = 6 \text{ mm}}$$